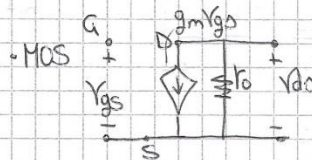
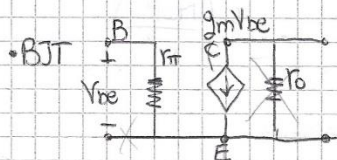


PUNTO DI LAVORO  $\Rightarrow$  CONTINUA  $\Rightarrow$  Condensatori  
DC circuiti aperti

Guadagno in  
tensione

$$A_v = \frac{V_{out}}{V} \cdot \frac{V}{V_{in}}$$

$\Rightarrow$  ALTERNATA  $\Rightarrow$  Condensatori  
AC circuiti chiusi + modelli



| BJT                                                                                    | MOS                                   |           |
|----------------------------------------------------------------------------------------|---------------------------------------|-----------|
| $I_C/V_T$                                                                              | $2I_D/V_{GS}-V_{TH}$                  | $g_m$     |
| $V_A/I_C$                                                                              | $1/nI_D$                              | $r_o$     |
| $V_A/V_T$                                                                              | $\frac{1}{n} \sqrt{\frac{2k_n}{I_D}}$ | $\mu F$   |
| $\beta F/g_m$                                                                          | $\infty$                              | $r_{\pi}$ |
| $V_{be} \leq 5mV$ $V_{gs} \leq 0.2[V_{GS}-V_{TH}]$ <small>cond piccolo segnale</small> |                                       |           |

$$A_v = \frac{V_{out}}{V_B} \cdot \frac{V_B}{V_{in}}$$

$$V_{BIA} = V_{GS}/V_{RE} + R_S/g_m V_{GS}/V_{RE}$$

$$V_{out} = -R_L g_m V_{GS}$$

$$g_m r_{\pi} = \beta F$$

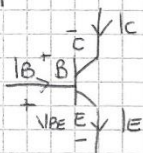
$$V_B = I_B r_{\pi} + (R_E \dots)$$

$$R_{IB} = \frac{V_B}{I_B}$$

$$V_B = V_I = \frac{R_{IB} R_S}{R_I + R_{IB} R_S}$$

$$V_{GS} = V_G, V_G = V_I \frac{R_S}{R_I + R_S}$$

BJT



• INTERDIZIONE BE OFF BC OFF

• SAT BE ON BC ON

• RAD BE ON BC OFF

$$10 < \beta F < 500$$

$$0.9 < \alpha F < 0.99$$

•  $V_{CE}$  è molto piccolo

$$\left. \begin{aligned} I_E &= (\beta F + 1) I_B \\ I_C &= \beta F I_B \\ I_E &= I_C + I_B \end{aligned} \right\} \beta F = \frac{\alpha F}{1 - \alpha F} = h_{FE} \text{ guadagno in corrente}$$

• RA1

BE OFF BC ON

$$V_{BE} = 0.7$$

$$0 < \beta R < 10$$

$$I_E = -\beta R I_B$$

$$I_E = \alpha R I_C$$

$$I_C = I_S \left[ e^{\frac{V_{BE}}{V_T}} - e^{\frac{V_{BC}}{V_T}} \right] - \frac{I_S}{\beta R} \left[ e^{\frac{V_{BC}}{V_T}} - 1 \right]$$

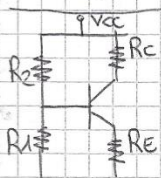
$$I_E = I_S \left[ e^{\frac{V_{BE}}{V_T}} - e^{\frac{V_{BC}}{V_T}} \right] + \frac{I_S}{\beta F} \left[ e^{\frac{V_{BE}}{V_T}} - 1 \right]$$

$$I_B = \frac{I_S}{\beta F} \left[ e^{\frac{V_{BE}}{V_T}} - 1 \right] + \frac{I_S}{\beta R} \left[ e^{\frac{V_{BC}}{V_T}} - 1 \right]$$

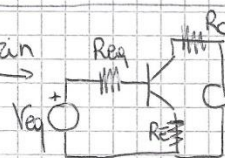
$$I_T = I_S \left[ e^{\frac{V_{BE}}{V_T}} - e^{\frac{V_{BC}}{V_T}} \right]$$

$$I_{snph} = \frac{q A D n_i^2}{W_B N_A}$$

$$I_{snph} = \frac{q A D p_n^2}{W_B N_D}$$



Theremin



$$R_{eq} = \frac{R_1 R_2}{R_1 + R_2}$$

$$V_{eq} = \frac{R_1}{R_1 + R_2} V_{cc}$$

$$T_F = \frac{W_B^2}{2 D_n}$$

$$C_D = \frac{I_T}{V_T}$$

$$V_{BC} = V_{BE} - V_{CE}$$

mobilità elettroni  $\mu_n = 1350 \text{ cm}^2/\text{Vs}$   
 lacune  $\mu_p = 550 \text{ cm}^2/\text{Vs}$

$$\frac{D_n}{\mu_n} = \frac{D_p}{\mu_p} = \frac{kT}{q} = V_T = 26 \text{ mV}$$

•  $K: \text{Boltzmann} = 8.62 \cdot 10^{-5}$   
 •  $q = 1.6 \cdot 10^{-19}$

$n \approx N_D$   
 $p \approx N_A$

$p = \frac{n_i^2}{N_D \approx n}$

ricombinazione  
 $R = rnp$   
 generazione  $G_i = r n_i^2$

$np = n_i^2$  → elettroni ionizzati

•  $\tau = \frac{1}{r N_A}$

•  $L_n = \sqrt{D_n \tau}$

regione di svuotamento  
 + grande - drogaggio

$n_i^2 = T^3 e^{-\frac{E_g}{2kT}}$

•  $T = 300 \text{ K}$

•  $E_g$  potenziale di banda proibita  
 ( $\approx 1.12$ )

conduttività

$\sigma = (n\mu_n + p\mu_p)q$

densità di corrente

$J = qEn(\mu_n + \mu_p)$

potenziale di giunzione  $\phi = V_T \ln \left( \frac{N_D N_A}{n_i^2} \right)$

→  $N_D x_n = N_A x_p$

DIODO



•  $V = 0 \Rightarrow I = 0$

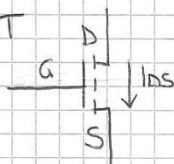
•  $V < 0$  PI  $\Rightarrow I = 0$

•  $V > 0$  PD  $\Rightarrow I = I_s (e^{\frac{V}{V_T}} - 1)$

$V = 0.6 \text{ V}$

$I_s = \frac{qSD_n}{L_n} \frac{n_i^2}{N_A}$

MOSFET



1. Conduzione  $V_{GS} > V_{TH}$

2. Saturazione  $V_{DS} \gg V_{GS} - V_{TH} \Rightarrow I_{DS} = \frac{K_n}{2} (V_{GS} - V_{TH})^2$  \*

3. LINEARE  $\Rightarrow I_{DS} = K_n ((V_{GS} - V_{TH})V_{DS} - \frac{1}{2}V_{DS}^2)$

↓ ma se  $V_{DS} \ll 2(V_{GS} - V_{TH}) \Rightarrow I_{DS} = K_n (V_{GS} - V_{TH})V_{DS}$

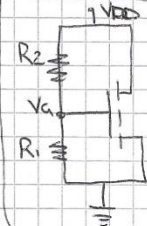
tensione di soglia

$V_{TH} = (2qF) + d \sqrt{\frac{2qN_A}{\epsilon} (2qF)}$

$K_n = \frac{C_{ox} \mu_n W}{L}$

•  $C_{ox} = \frac{\epsilon}{d}$

\*  $I_{DS} = K_n (V_{GS} - V_{TH})^2 (1 + nV_{DS})$



$V_G = \frac{R_1}{R_2 + R_1} V_{DD}$

Specchio di corrente

$V_{GS}^1 = V_{GS}^2$   
 $\Rightarrow I_{DS}^1 = I_{DS}^2$